Analog Filters Using MATLAB — Corrections, version 2016-04-25

Replace in all MATLAB programs ( ) with («) and (—) with (-)

#### Page 33,

Equation (2.18) ..cos(,,(N+2k-1)/2N)

Note that  $\sigma_p < 0$  for all poles and all of the coefficients in the denominator **have the same sign** in a stable analog filter.

#### Page 34 and 35 [GLP, ZLP, PLP] =

Page 42 Parameters have been changed to [G, Z, R\_ZEROS, P] = CH\_II\_POLES(Wc, Ws, Amax, Amin, N)

Page 44 left column: (2.21

(2.21) be replaced with (2.27)

Page 45 Equation (2.44): the denominator for r\_{pk} should read ...[(1/N)asinh(K)]

Page 47 Parameters have been changed to [G, Z, R\_ZEROS, P, Wsnew] = CA\_POLES(Wc, Ws, Amax, Amin, N)

### Page 56

line 11-13 in the MATLAB program should be Att = MAG\_2\_ATT(H); axis([0 8 0 100]), subplot('position', [0.1 0.4 0.88 0.5]); PLOT\_ATTENUATION\_S(W, Att) hold on color = [0.7 0.7 0.7]; % Gray V = axis; patch([V(1) Wc Wc V(1)], [Amax Amax V(4) V(4)], color); patch([wstep(1) wstep(1) wstep(2) wstep(2) V(2) V(2)], [0 Amin(1) Amin(2) Amin(2) 0], color);

### Page 59

Eq(2.58) is only valid for allpole filters

Page 61

[GLP, ZLP, PLP] = BW\_POLES(Omegac, Omegas, Amax, Amin, NLP)

Page 62

GLP = 1.592185381683073e+23

Page 67 line 7 should read LP-BS transformation

#### Page 69

and lowpass filters using the LP-BS transformation is

**Page 69** [GLP, ZLP, R\_ZEROSLP, PLP, Wsnew] = CA\_POLES(Omegac, Omegas, Amax, Amin, NLP);

### Page 72

add at the end of the program for Example 2.10 patch([Wc1 Wc2 Wc2 Wc1], [Amax Amax 100 100], color);

### Page 75

Problem 2.24  $\omega = 2$  Mrad/s and  $r_p = 10$  Mrad/s. Problem 2.36  $\omega_{c2} = 15$  krad/s **Page 76** Problem 2.39  $\omega_{c1} = 2\pi$  48.5 rad/s  $\omega_{c2} = 2\pi$  51.5 rad/s  $\omega_{s1} = 2\pi$  49.5 rad/s  $\omega_{s2} = 2\pi$  50.5 rad/s

# Page 81

 $|C(s)|^2$  is proportional to the ratio

### Page 95

line 14 replace Att with Anorm

### Page 96

line 18 replace Att with Anorm

«

**Page 97** line 4 change [ ....] to (....) and change N to Norder move line 6 to after line 3 line 8 replace KI with K line 12 replace Att with Anorm Example  $3.7 A_{min} = 40$  dB

### Page 98 should read

new line 9 Norder = 5; % We select a 5th-order filter line 10 [G, Z, R\_ZEROS, P, Wsnew] = CA\_POLES(Wc, Ws, Amax, Amin, Norder); line 12 [L, C, Rs, RL, Wo, K] = CA\_LADDER(G, Z, R\_ZEROS, P, Wc, Ws, Rs, RL, Ladder); line 16 Anorm = MAG\_2\_ATT(2\*H); % Normalize attenuation to 0 dB

### Page 117

A useful program for this step is HURWITZ.

### Page 152

Eq(3.63) replace all L s with C s and vise versa Cauer II structure should be



Page 123 Example 3.20

Determine the element values in a sixth-order allpass filter built of cascaded bridged-*T* networks which equalizes the group delay of the ladder network in Example 2.4 when  $R_s = R_L = 1000 \Omega$ .

The poles of the allpass filter were determined by the program in Example 2.11-determined to

 $s_{p1,2} = -7.576348 \pm j 6.5452758$  krad/s  $s_{p3,4} = -7.350304 \pm j19.284823$  krad/s  $s_{p5,6} = -6.903609 \pm j32.393479$  krad/s

From Equation (3.67) we obtain the element values in the lattice structures. We get using:  $1/RC_2 = -2 Re\{s_p\}$  and  $1/L_2C_2 = r_p^2$  and  $R = 1 k\Omega$ . The Table have new values!

Bridged-T	$L_1[mH]$	$L_2[mH]$	$C_1[nF]$	$C_2[nF]$
1	65.99485	151.1616	151.1616	65.99485
2	68.0244	34.51403	34.51403	68.0244
3	72.42589	12.58637	12.58637	72.42589

### Page 130

Problem 3.16 should read: Realize an *LC* ladder that meets the same specification as in Problem 3.15, but of Cheby-shev I type.

Problem 3.20 should read

.....  $\omega_{s1} = 11.6$  Mrad/s, and  $\omega_{c2} = 311.6$  Mrad/s.

#### Page 131

3.26 .....terminated  $\pi$  ladder network with Page 137 where the function  $\tan(\omega \tau)$  is periodic with period ....

#### Page 141

### In Example 4.2. $\tau = 0.25$ ns

and  $\omega_c T = 2,, 300 \ 10^6 \ 0.25 \ 10^{-9} = 0.15$ , rad

$$\left|H(e^{j\omega T})\right|^{2} = \frac{1}{1 + \left(\frac{\sin\left(\frac{\omega T}{2}\right)}{\alpha}\right)^{2N}}$$

where  $\alpha = \varepsilon^{-\frac{1}{N}} \sin\left(\frac{\omega_c T}{2}\right) \dots$ 

with period ". The impedance...

# Page 142

In Example 4.3.  $\tau = 0.25$  ns and  $\omega_c T = 2,, 300 \times 10^6 \times 0.25 \times 10^{-9} = 0.15$ , rad Figure 4.10 The x-axis should be from 0 to ,, The function RICHARDS EQ has an error do not yiels a correct passband!

### Page 143

Figure 4.11 The x-axis should be from 0 to "

#### Page 144

$$Z_1 = \frac{L_1 R_0}{\Omega_c} = 3.1147435 \ \Omega$$
$$Z_2 = \frac{\Omega_c R_0}{C_2} = 0.160527 \ \Omega \qquad Z_3 = \frac{L_3 R_0}{\Omega_c} = 3.1147435 \ \Omega$$

### Page 146

Example 4.5 change to a Chebyshev I filter

#### Page 146

line -7:  $X = \frac{K}{1 - (\frac{K}{Y_0})^2}$ 

Page 152 Problem 4.8 the relative 3-dB bandwidth

### Page 152

Equation(5.74) simplifies for ideal amplifiers to  $Z_{in} = Z_1 Z_3 Z_5 / Z_2 Z_4$ 

#### Page 200

$$Q_{nominal} = \frac{-r_p}{2\sigma_p} = \frac{-\sqrt{(5\pi)^2 + (50\pi)^2}}{2 \cdot (-5\pi)} = 5.0249378$$

Page 201

 $D(s) + \frac{E(s)}{A} =$ 

Page 201 Fig. 7.10 Tow-Thomas

Page 201 6.5.3.7 NF2 Sections

### Page 205

where the amplifier has a positive gain of  $K = (1 + R_8/R_7) > 1$ . We shall later discu

Page 206 delete the line a positive gain of  $K = (1 + R_8/R_7) > 1$ . We shall

**Page 213** Spreads in passive elements are  $\propto Q^2$ .

Page 224 Table, second line HP 0  $V_{in}$   $V_{in}$   $R_2 = R_1$  Page 237 7.3.2 Flicker Noise

**Page 245** Fig. 7.14 Coupled form of type FLF

**Page 260** Line 3, second column: example  $k = 10^5$  [1/s].

Page 273 output wave is  $B_2$ , which corresponds to the output voltage  $V_{B2}$ . Page 279 the marked minus signs across the nodes..

Page 279 Hence, the sign of V<sub>7</sub> is changed

**Page 280** Figure 10.9 Interchange the inputs to the rightmost amplifier

Page 281 determined by comparing the circuits

Page 282 from the node that is

## Page 289

10.1 .. leapfrog filter

### Pages 309 and 310

BESSEL\_ORDER 59 BESSEL POLES BESSEL LADDER BP 2 LP SPEC BS 2 LP SPEC BW LADDER 94, 95 BW ORDER 34 BW\_POLES 34 BW SINGLY LADDER CA POLES 50 CA\_B\_POLES 52 CA\_C\_POLES 53 CA LADDER 97 CA MIN Q POLES CA ORDER 48 CH I C POLES 53 CH I LADDER 96 CH I POLES 39 CH\_I\_SINGLY\_LADDER CH II B POLES 52 CH II LADDER 96 CH II POLES 46 CH\_ORDER 39, 44

CIRCULATOR\_THREE\_BP 271 CIRCULATOR\_THREE\_LP 271 COMPLETE\_ELLIPTIC\_INTEGRAL EQ\_TG\_LP\_S 73 HURWITZ 113 HURWITZ POLY 32 HURWITZ ROOTS 32 LADDER\_2\_H 96  $LP_2_HP_LADDER$ LP\_LADDER PART\_FRACT\_EXPANSION 120 PLOT A TG S 35 PLOT\_ATTENUATION\_S PLOT\_h\_s\_S 36 PLOT HP SPEC S PLOT\_IMPULSE\_RESPONSE\_S PLOT\_LP\_SPEC\_S PLOT\_MAG\_PHASE\_S PLOT PHASE S PLOT PZ S 35 PLOT\_STEP\_RESPONSE\_S PLOT\_TG\_S POLE\_PLACER\_BP\_EQ\_S 56 POLE\_PLACER\_BP\_MF\_S 56, 71 POLE\_PLACER\_HP\_EQ\_S 56 POLE PLACER HP MF S 56 POLE PLACER LP EQ S 56 POLE\_PLACER\_LP\_MF\_S 56 POLY\_AT\_X POLY\_PRIM POLYADD POLYMULT POLYSUB PRAXIS PRB 249 PZ\_2\_FREQ\_S 35 PZ 2 G SYM BP S 65 PZ\_2\_G\_SYM\_BS\_S 69 PZ\_2\_HP\_S 61 PZ\_2\_IMPULSE\_RESPONSE\_S 36 PZ 2 MAG S PZ 2 PHASE S PZ\_2\_STEP\_RESPONSE\_S 36 PZ\_2\_TG\_S 35 RICHARDS\_EQ 141 RICHARDS\_MF 141 **RICHARDS REACTANCE 140** ROOTS 2 POLY T LADDER 2 PI UNIQUE\_ROOTS xtick ytick ZIN\_LADDER